



that one “correct” value is appropriate at all times or for all conditions.

The “correct” value varies based on the specific conditions of the lab at a given point in time. For example, if a spill of a solvent or volatile chemical occurs, or chemists are doing work on a bench top that should be done in a hood, a higher room air change rate is desirable. In a spill situation, a rate far above 6 or 8 ACHs, such as 16 ACHs, can provide superior dilution performance at the time of the incident and for a period of time afterwards. When the situation calls for it, a higher air change rate is much more effective in reducing contaminant levels quickly. However, the majority of the time, under normal operating conditions, lab room air is typically clean, and a minimum of 2 ACH would be “correct.” Diluting cleanroom air with clean supply air achieves no benefit and wastes significant amounts of energy.

Consequently, the best theoretical approach regarding minimum air change rates for labs would be to determine the rate based on the real time quality of the air in the laboratory. This would allow airflow in a lab to vary based on all the situational factors affecting lab airflow, as opposed to only the status of the hoods and the thermal load. Implementing a dynamic approach to controlling minimum air change rates requires the ability to measure a unique set of indoor air parameters, such as total volatile organic compounds (TVOCs), particles, carbon dioxide, and humidity, and to integrate this information with the building management system.

Until now, such an approach similar to demand control ventilation (DCV) but applied to laboratories and vivariums, has not been feasible or cost effective primarily due to the quality and quantity of sensors necessary to safely implement this approach. In addition, the associated calibration and maintenance costs rendered it impractical to populate a large number of sensors throughout a facility.

### A New Technology Provides a Solution

A new sensing architecture has been developed that can now implement the dynamic control of laboratory room air change rates in a practical, reliable, and cost effective manner. This new sensing approach changes the age old paradigm of sensing and minimizes calibration and maintenance expenses. Instead of placing multiple sensors in each sensed space or area of a building, this networked system routes packets or samples of air sequentially in a multiplexed fashion to a shared set of sensors. Every 30 to 40 seconds, a sample of air from a different area is routed on a common air sampling backbone to

the same set of sensors, known as a sensor suite, for measurement. These sequential measurements are then “de-multiplexed” for each sampled area to create distinct sensor signals used for traditional monitoring and control. Typically, 15 to 20 areas can be sampled with one set of sensors, approximately every 15 minutes depending on the requirements for those spaces.

Calibration and maintenance expense is minimized due to the limited number of sensors and their centralized grouping in one location. The calibration process is easily accomplished through an exchange program whereby a set of factory calibrated sensors from the manufacturer periodically replaces the onsite sensors, such as every six months. The system is therefore assured to operate at peak performance with minimal or no disruption to the facility’s operation.

A key innovation in this multiplexed sensing system is the development of a structured cable containing low voltage power and signal conductors, data communications, and a unique, one quarter inch hollow conduit. This sample conduit provides the transport media through which the air packets are passed one after another, similar to data packets on the communications network used in building management systems. To substantially eliminate air packets from contaminating subsequent packets, the inner walls of the air sample conduit are made of a mixture of an inert fluoropolymer and a unique nanotechnology material known as carbon nanotubes. These micron long chains of carbon atoms form inert, electrically conductive strands that, when mixed with the plastic fluoropolymer, form an electrically conductive matrix that prevents the buildup of static charges that might impede the flow of particles and aerosols. The resultant sample conduit can accurately transport and preserve the air sample’s properties to support accurate measurement up to 500 feet away from the centrally located sensor suite.

This multiplexed sensing approach (Figure 1) can measure almost any air parameter of interest. For laboratories, the use of a PID, or photo-ionization detector type of TVOC sensor, is very beneficial for accurately detecting literally hundreds of commonly used laboratory chemicals that can volatilize and become a safety concern. Combining this sensor with a laser-based particle counter to identify aerosol vapors, plus other specialty sensors affords detection of the majority of airborne chemicals of concern.

In this dilution ventilation control concept, when an increase in contaminants in a space is detected, the airflow in the room is increased as appropriate up to a max-

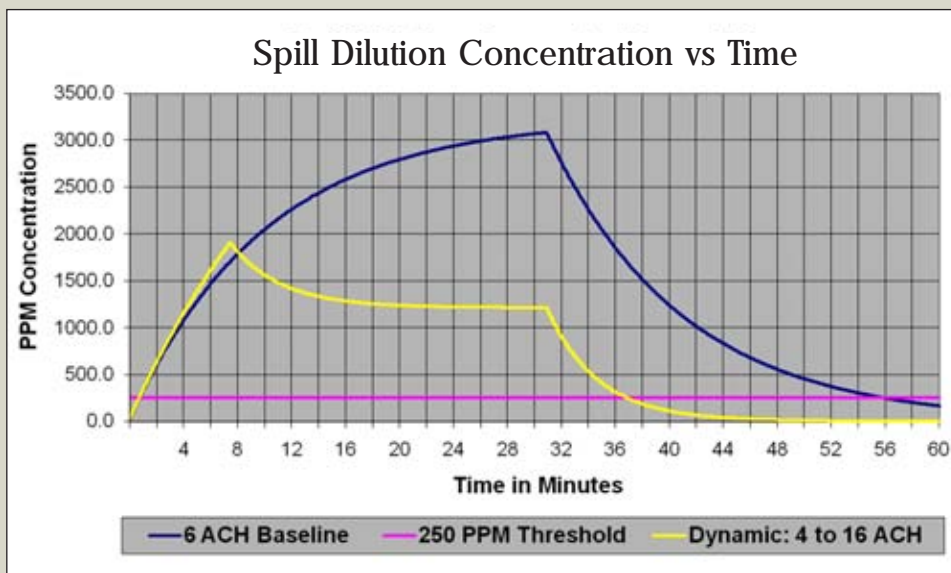


Figure 2: Comparison of Dilution Rates of Acetone as a Function of Air Change Rates

The graph shown in Figure 2 illustrates the significant benefits of operating at higher ACH rates during a spill. Figure 2 illustrates what happens during a National Institutes of Health (NIH) handbook dilution ventilation test of spilling a 1.5 liter container of acetone on the floor of a single 200 sq. ft. lab module.<sup>2</sup>

The figure of merit evaluated by NIH is the length of time it takes to reduce the contaminant to a safe level, shown in Figure 2 as 250 PPM or 1/3 of the threshold limit value (TLV). After approximately 7.5 minutes from the point of occurrence, the dynamic control system senses a spill and increases the air change rate from 4 ACH to 16 ACH, which

reduces the peak concentration reached versus the 6 ACH baseline ventilation case. Additionally, after 31 minutes, the solvent has evaporated and the dynamic system takes only five minutes to reach the 250 PPM threshold, whereas the 6 ACH baseline takes five times longer or 25 minutes to reach this same level. Even more interesting, is that after one hour the dynamic dilution control system reduces the background level of acetone vapors to 0.53 PPM whereas the 6 ACH baseline is still at 169.0 PPM or 320 times greater.

imum level such as 15 ACHs or the design capability of the room's airflow control devices. The lower value of the dynamic range when the air in the lab is "clean" can be set to 4 ACH (Occupational Safety and Health Administration or OSHA guidelines recommend 4 to 12 ACH).<sup>1</sup> For additional savings, a nighttime or unoccupied level of 2 ACH can also be implemented. For less critical labs or support rooms, 2 ACHs could be used as the minimum level for all times. Although a value such as 2 ACHs at first glance might seem low, analyzed further, it is more than three times the typical occupied office outside air ventilation level.

It is important to note that no set of sensors will detect every possible compound that can be used in a laboratory. However, with the sensors previously described, the vast majority (90 to 95%) of the chemicals of concern will be detected, allowing the air change rate to be appropriately increased. As a result, for the vast majority of spills or chemical releases, it is preferable for safety reasons to increase a lab's airflow rate from 6 or 8 ACH to 15 ACH. The remaining 5 to 10% of the time, when a chemical release is not detectable, the lab will still operate at the OSHA minimum guideline of 4 ACH. Varying air change rates as the situation demands thus provides a better overall approach compared to operating at 6 or 8 ACH *all* the time, regardless of whether a spill or accidental release of chemicals occurs in the lab.

Controlling Air Change Rates in Vivariums

Regarding vivariums, this approach is an excellent means to both safely vary and oftentimes reduce air changes, while providing real time monitoring and documentation of the quality of the room environment in which the animals are housed. Air quality problems that could affect research results can be quickly detected and remedied before the animals are substantially impacted. The ability to reduce an animal room's air changes from perhaps 10 or even 20 ACH to 6 or 8 ACH is not only now practical but allowed.

The Institute for Laboratory Animal Research (ILAR) guide used by the Association for Assessment and Accreditation of Lab Animal Care (AAALAC) for vivarium accreditation permits lower air change rates as long as good, or specifically non-harmful, levels of

reduces the peak concentration reached versus the 6 ACH baseline ventilation case. Additionally, after 31 minutes, the solvent has evaporated and the dynamic system takes only five minutes to reach the 250 PPM threshold, whereas the 6 ACH baseline takes five times longer or 25 minutes to reach this same level. Even more interesting, is that after one hour the dynamic dilution control system reduces the background level of acetone vapors to 0.53 PPM whereas the 6 ACH baseline is still at 169.0 PPM or 320 times greater.

room air quality are maintained. In particular, the *ILAR Guide to the Care and Use of Laboratory Animals* is a performance-based standard that specifically states that fixed air change rate guidelines such as 10 to 15 ACH although being generally accepted, "...might pose a problem by over ventilating a secondary [room] enclosure that contains few animals and thereby wasting energy or by under ventilating a secondary enclosure that contains many animals and thereby allowing heat and odor accumulation."<sup>3</sup> Additionally, the *ILAR Guide* states that lower room ventilation rates can be appropriate, "...provided that they do not result in harmful or unacceptable concentrations of toxic gases, odors, or particles in the primary [animal cage] enclosure."<sup>3</sup> By directly measuring and controlling room particle levels, as well as odors/TVOCs and ammonia, good room air quality levels can be maintained energy efficiently.

#### Application Examples

A case study example of the impact of dynamically varying air changes in labs and vivariums can be illustrated by the GreenLab project in Seattle, Washington. GreenLab is a prototype lab project in the design process that is being developed by Vulcan, Inc. The architect is Perkins + Will, and the consulting engineer is Keen Engineering (now Stantec Engineering). The 215,000 sq. ft. project is called GreenLab to reflect Vulcan's interest in making this lab as energy efficient and sustainable as possible. A full concept design and thorough energy analysis was completed on this project, including the use of the previously described multiplexed sensing system to dynamically vary the air changes in both a 75,000 sq. ft lab area and a 25,000 sq.

ft. animal facility. This analysis assumed changing the previously fixed design air change rate of 8 ACH to a variable rate of between 4 and 16 ACH in the lab areas, and from a fixed 15 ACH to a range of from 8 to 16 ACH in the vivarium. The result was a \$250,000 reduction in annual energy costs or 20% of the total utility bill for the entire

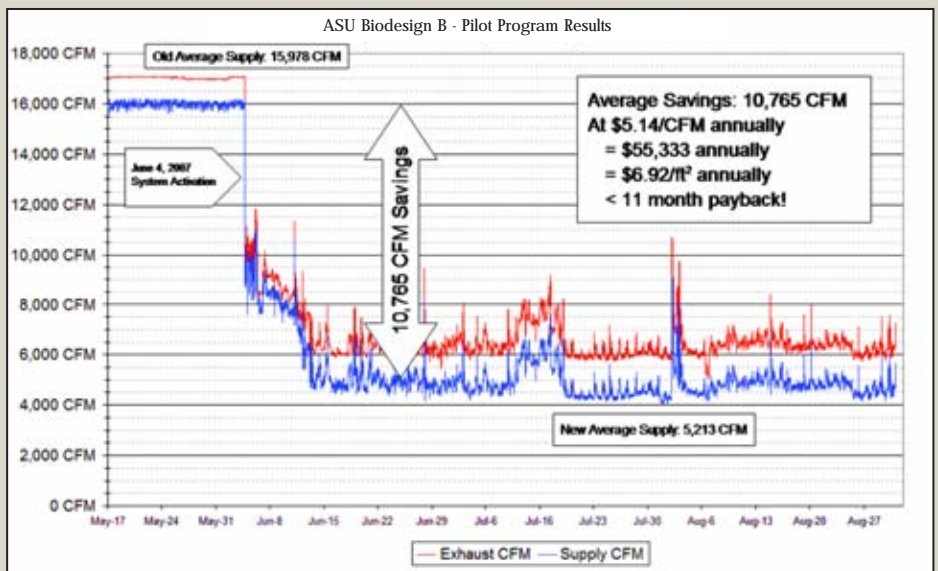


Figure 3: ASU Biodesign-B Retrofit Pilot Project Airflow Savings Results

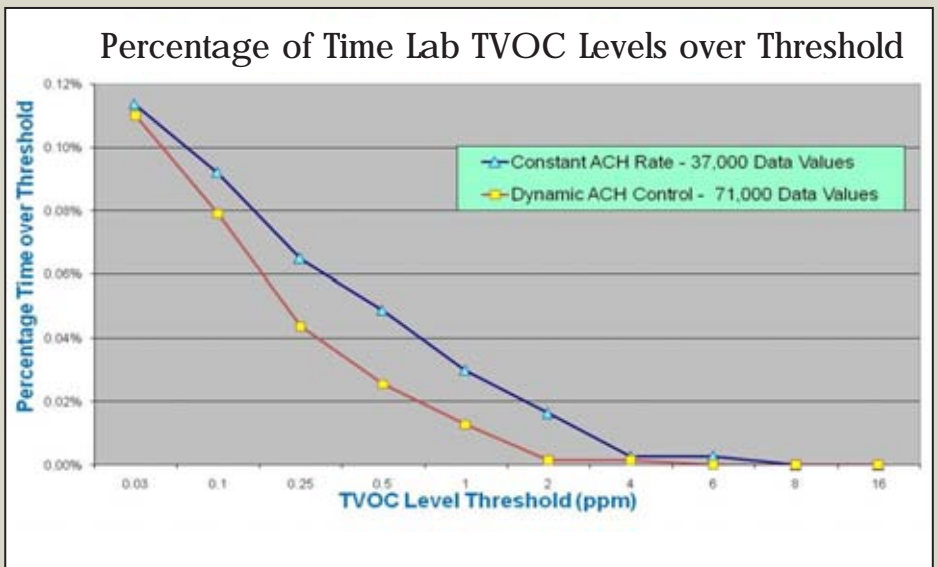


Figure 4: ASU Biodesign-B Project Average TVOC "Before and After" Results

215,000 sq. ft. facility. This represented a 1.5 year pay-back in Seattle's mild climate and according to the design team, the IEQ monitoring and dynamic ACH control system represented, "the single largest energy conservation measure of the project."

This system also generated a net reduction of first cost in the GreenLab project. For the 75,000 sq. ft. lab area, a gross reduction of approximately \$1,025,000 of HVAC system first cost was achieved by reducing the minimum air change levels in the labs and using a more realistic thermal load assessment. The result was a reduction in the design capacity of the HVAC system from supplying all labs simultaneously with approximately 16 ACH of air flow to a reduced level of 9 ACH. In total, the gross first cost reduction in the HVAC system (air handlers, exhaust fans, furnace, VFDs, and chiller) was approximately \$13.68 per square feet of lab space.

An installed case study example of this approach can be seen at the new Biodesign-B building at Arizona State University that was recently certified as a LEED Platinum facility. A pilot project to dynamically vary air changes using multiplexed sensing was installed as a retrofit in mid 2007. The building was initially designed with a minimum ventilation rate of 12 ACH. It was decided to reduce the air change rate by a factor of 3 down to 4 ACH when the lab is clean, and to increase the airflow to between 16 to 18 ACH when contaminants are sensed in the lab. Figure 3 shows the results of this control approach for 11 lab rooms. The energy savings from this approach are quite significant as shown with a payback of less than one year even using conservative energy numbers.

An interesting aspect of the pilot as indicated in the graph in Figure 3 is that the lab airflows initially did not reach the final level and for two weeks, were higher than expected. This turned out to be caused by thermostats that were open to the wall cavity. As a result, the negative lab environment drew warm wall cavity air into the room through the thermostat causing incorrect readings and overcooling the room. This preexisting problem had not been noticed before. However, when the thermostat openings were sealed over a two week period, the airflows dropped to the final levels shown. As seen in this example, dropping lab airflows typically

points out some existing problems that often times with some retrocommissioning efforts can ensure both the expected savings or find pre-existing problems that were causing additional energy waste.

In terms of the safety impact of the new control approach on the lab, Figure 4 shows the cumulative average level of TVOCs in the ASU labs both before and after the retrofit was completed. As can be seen by the data, even though the normal minimum lab air change rate was reduced by a factor of three, the ability to significantly increase the air change rate above the previous minimum rate rapidly purges the lab when contaminants are detected. This resulted in a significant reduction of VOC contaminants in the lab areas as shown by Figure 4.

In addition to safely saving energy in laboratory and vivarium facilities, multiplexed sensing technology can also be used in non-lab areas such as offices, classrooms, healthcare facilities, and many other buildings where the control of outside air is important to save energy. Strategies such as demand control ventilation and other outside air control approaches such differential enthalpy control that can require significant numbers of sensors can now be applied accurately, cost effectively, and reliably for all types of facilities.

## References

1. Occupational Safety and Health Administration (OSHA) *29 CFR Part 1910.1450*. Washington DC: U.S. Government Printing Office, 2001. p.492.
2. National Institutes of Health *Design Policy and Guidelines* Office of Research Facilities Spring 2003 Mechanical F.64-67.
3. Association for Assessment and Accreditation of Lab Animal Care. *Guide for the Care and Use of Laboratory Animals* (NRC1996), p.32.

**Gordon P. Sharp** is the founder and Chairman for Aircuity, Inc. Mr. Sharp is also the founder and former CEO of Phoenix Controls and has more than 25 U.S. patents to his name.

Aircuity, Inc., 39 Chapel Street, Newton, MA 02458; (617) 641-8800; gsharp@aircuity.com; www.aircuity.com.